

Research Article

# Radiative Heat and Mass Transfer Effects on Natural Convection Couette Flow through a Porous Medium in the Slip flow Regime

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## Abstract

The objective of this paper is to analyze the effect of radiative heat and mass transfer on unsteady natural convection couette flow of a viscous incompressible fluid in the slip flow regime in presence of variable suction and radiative heat source. The governing equations of the flow field are solved employing perturbation technique and the expressions for the velocity, temperature, concentration distribution, skin friction and the rate of heat transfer i.e. the heat flux in terms of Nusselts number  $N_u$  are obtained. The effects of the pertinent parameters such as suction parameters  $\alpha_1, \alpha_2$ ; Grashof number for heat and mass transfer  $G_r, G_c$ ; slip flow parameters  $h_1, h_2$ ; radiation parameter  $F$ , permeability parameter  $K_p$ , Schmidt number  $S_c$ , Prandtl number  $P_r$ , etc. on the flow field have been studied and the results are presented graphically and discussed quantitatively. **Copyright © IJRETR, all right reserved.**

**Keywords:** Radiative heat; Mass transfer; Natural convection; Couette flow; Variable suction; Permeability.

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## Introduction

In recent years the effect of radiation on flow problems with heat transfer has been given much importance in different fields of engineering and technology. Many engineering processes occur at high temperatures and the knowledge of radiation heat transfer has become very important for the design of pertinent equipments such as nuclear power plants, gas turbines and various propulsion devices for aircrafts, missiles, satellites and space vehicles. At high operating temperature, radiation effect is very significant. In view of the above interests a series of investigations have been made by different scholars.

Govindarajulu [1] discussed hydromagnetic couette flow with time-dependent suction. Sattar and Alam [2] analyzed thermal diffusion as well as transpiration effect on MHD free convection and mass transfer flow past an accelerated vertical porous plate. Sattar and Kalim [3] studied the unsteady free convection interaction with thermal radiation in a boundary layer flow past a vertical porous plate. Attia and Kotb [4] reported MHD flow between two parallel plates with heat transfer. Raptis and Perdikis [5] discussed radiation and free convection flow past a moving plate. Nagaraju *et al.* [6] investigated simultaneous radiative and convective heat transfer in a variable porosity medium. Sreekanth *et al.* [7] described transient MHD free convection flow of an incompressible viscous dissipative fluid. Chamkha [8] analyzed MHD flow of a uniformly stretched vertical permeable surface in presence of heat generation /absorption and chemical reaction.

Cookey *et al.* [9] discussed the influence of viscous dissipation and radiation on unsteady MHD free convection flow past an infinite heated vertical plate in a porous medium with time dependent suction. Gokhale and Alsamman [10] estimated the effects of mass transfer on the transient free convection flow of a dissipative fluid along a semi-infinite vertical plate with constant heat flux. Singh and Gupta [11] investigated the MHD free convective flow of viscous fluid through a porous medium bounded by an oscillating porous plate in the slip flow regime with mass transfer. Das and his associates [12] estimated numerically the mass transfer effects on unsteady flow past an accelerated vertical porous plate with suction. Ibrahim *et al.* [13] analyzed the effect of chemical reaction and radiation absorption on the unsteady MHD free convection flow past a semi-infinite vertical permeable moving plate with heat source and suction. Das [14] investigated the effect of suction and injection on MHD three dimensional couette flow and heat transfer through a porous medium. Das and his co-workers [15] discussed the hydromagnetic convective flow past a vertical porous plate through a porous medium with suction and heat source.

The objective of this paper is to analyze the effect of radiative heat and mass transfer on unsteady natural convection couette flow of a viscous incompressible fluid in the slip flow regime in presence of variable suction and radiative heat source. The governing equations of the flow field are solved for the velocity, temperature, concentration distribution, skin friction and the rate of heat transfer and the effects of the various flow parameters on the flow field have been studied and the results are presented graphically and discussed quantitatively.

## 2. Formulation of the problem

We consider a two dimensional unsteady free convective flow of a viscous incompressible fluid between two vertical parallel porous plates placed at a distance  $h$  apart in the slip flow regime in presence of variable suction and radiative heat source. Let the medium between the plates be filled with a porous material of permeability

$$K'(t') = K'_0 \left( 1 + \varepsilon B e^{-\omega' t'} \right), \quad (1)$$

and a time dependent suction

$$v'(t') = -v'_0 \left( 1 + \varepsilon A e^{-\omega' t'} \right) \quad (2)$$

be applied at the plate  $y=0$  and the same injection velocity be applied at the plate  $y=1$ . We choose  $x$ -axis along the plate and  $y$ -axis normal to it. Under the above conditions the equations governing the flow are:

Momentum equation:

$$\frac{\partial u'}{\partial t'} - v'_0 \left( 1 + \varepsilon A e^{-\omega' t'} \right) \frac{\partial u'}{\partial y'} = g\beta(T' - T'_h) + g\beta^*(C' - C'_h) + \nu \frac{\partial^2 u'}{\partial y'^2} - \frac{\nu}{K'(t')} u', \quad (3)$$

Energy equation:

$$\frac{\partial T'}{\partial t'} - v'_0 \left( I + \varepsilon A e^{-\omega t'} \right) \frac{\partial T'}{\partial y'} = \frac{k}{\rho C_p} \frac{\partial^2 T'}{\partial y'^2} - \frac{I}{\rho C_p} \frac{\partial q_r}{\partial y'}, \quad (4)$$

Concentration equation:

$$\frac{\partial C'}{\partial t'} - v'_0 \left( I + \varepsilon A e^{-\omega t'} \right) \frac{\partial C'}{\partial y'} = D \frac{\partial^2 C'}{\partial y'^2}. \quad (5)$$

The boundary conditions of the problem are:

$$u' - U_1 = L_1 \frac{\partial u'}{\partial y'}, \frac{\partial T'}{\partial y'} = -\frac{q}{k}, \frac{\partial C'}{\partial y'} = -\frac{m}{D} \quad \text{at } y' = 0,$$

$$u' - U_2 = L_2 \frac{\partial u'}{\partial y'}, T' = T'_h, C' = C'_h \quad \text{at } y' = h, \quad (6)$$

where  $L_1 = \frac{(2 - \mu_1)}{\mu_1} L$ ,  $L$  being the mean free path and  $\mu_1$ , the Maxwell's reflection coefficient.

The radiative heat flux  $q_r$  is given by

$$\frac{\partial q_r}{\partial y'} = 4(T' - T'_h)I, \quad (7)$$

where  $I = \int k_{\lambda w} \frac{\partial e_{b\lambda}}{\partial T} d\lambda$ ,  $k_{\lambda w}$  is the absorption coefficient at the wall,  $e_{b\lambda}$  is Planck's function and  $\lambda$  is the frequency,  $u'$  is the velocity,  $T'$  is the temperature,  $C'$  is the concentration,  $\beta$  is the volumetric coefficient of expansion for heat transfer,  $\beta^*$  is the volumetric coefficient of expansion for mass transfer,  $k$  is the thermal conductivity,  $\nu$  is the kinematic viscosity,  $C_p$  is the specific heat at constant pressure,  $D$  is the molecular diffusivity,  $g$  is the acceleration due to gravity,  $A$  and  $B$  are the real positive constants,  $t$  is the time and  $\varepsilon$  is a small positive number such that  $\varepsilon A \ll 1$  and  $\varepsilon B \ll 1$ .

Introducing the following non-dimensional variables and parameters,

$$y = \frac{y'v'_0}{\nu}, t = \frac{t'v'_0{}^2}{\nu}, \omega = \frac{\nu\omega'}{v'_0{}^2}, u = \frac{u'}{v'_0}, \nu = \frac{\eta_0}{\rho}, K_p = \frac{v'_0{}^2 K'_0}{\nu^2}, \theta = \frac{kv'_0(T' - T'_h)}{\nu q'}, C = \frac{Dv'_0(C' - C'_h)}{\nu m},$$

$$P_r = \frac{\rho\nu C_p}{k}, G_r = \frac{\nu^2 g\beta q}{kv'_0{}^4}, G_c = \frac{\nu^2 g\beta^* m}{Dv'_0{}^4}, F = \frac{4\nu I}{\rho C_p v'_0{}^2}, S_c = \frac{\nu}{D}, \alpha_1 = \frac{U_1}{v'_0}, \alpha_2 = \frac{U_2}{v'_0}, R = \frac{v'_0 h}{\nu},$$

$$h_1 = \frac{L_1 v'_0}{\nu}, h_2 = \frac{L_2 v'_0}{\nu} \quad (8)$$

in Equations (3)-(5), we get the following non-dimensional equations

$$\frac{\partial u}{\partial t} - \left( 1 + \varepsilon A e^{-\omega t} \right) \frac{\partial u}{\partial y} = G_r \theta + G_c C + \frac{\partial^2 u}{\partial y^2} - \frac{u}{K_p \left( 1 + \varepsilon B e^{-\omega t} \right)}, \quad (9)$$

$$\frac{\partial \theta}{\partial t} - (1 + \varepsilon A e^{-\omega t}) \frac{\partial \theta}{\partial y} = \frac{1}{P_r} \frac{\partial^2 \theta}{\partial y^2} - F \theta, \quad (10)$$

$$\frac{\partial C}{\partial t} - (1 + \varepsilon A e^{-\omega t}) \frac{\partial C}{\partial y} = \frac{1}{S_c} \frac{\partial^2 C}{\partial y^2}, \quad (11)$$

where  $G_r$  and  $G_c$  respectively are the Grashof number for heat and mass transfer,  $K_p$  is the permeability parameter,  $P_r$  is the Prandtl number,  $F$  is the radiation parameter,  $S_c$  is the Schmidt number,  $\alpha_1$  and  $\alpha_2$  are the suction parameters and  $h_1$  and  $h_2$  are the slip flow parameters.

The corresponding boundary conditions now reduce to:

$$u = \alpha_1 + h_1 \frac{\partial u}{\partial y}, \quad \frac{\partial \theta}{\partial y} = -1, \quad \frac{\partial C}{\partial y} = -1 \quad \text{at } y = 0, \\ u = \alpha_2 + \frac{\partial u}{\partial y}, \quad \theta = 0, \quad C = 0 \quad \text{at } y = h. \quad (12)$$

### 3. Method of Solution

We now wish to seek the solutions for Equations (9)-(11) under boundary condition (12) for a particular case  $R=1$ , which is valid for an incompressible fluid. In order to solve Equations (9)-(11), we assume

$$u(y, t) = u_0(y) + \varepsilon u_1(y) e^{-\omega t} + O(\varepsilon^2), \quad (13)$$

$$\theta(y, t) = \theta_0(y) + \varepsilon \theta_1(y) e^{-\omega t} + O(\varepsilon^2), \quad (14)$$

$$C(y, t) = C_0(y) + \varepsilon C_1(y) e^{-\omega t} + O(\varepsilon^2). \quad (15)$$

Using Equations (13)-(15) in Equations (9)-(11), we get the following zeroth order and first order equations:

Zeroth order:

$$-\frac{\partial u_0}{\partial y} = G_r \theta_0 + G_c C_0 + \frac{\partial^2 u_0}{\partial y^2} - \frac{u_0}{K_p}, \quad (16)$$

$$-\frac{\partial \theta_0}{\partial y} = \frac{1}{P_r} \frac{\partial^2 \theta_0}{\partial y^2} - F \theta_0, \quad (17)$$

$$-\frac{\partial C_0}{\partial y} = \frac{1}{S_c} \frac{\partial^2 C_0}{\partial y^2}, \quad (18)$$

First order:

$$-\omega u_1 - A \frac{\partial u_0}{\partial y} - \frac{\partial u_1}{\partial y} = G_r \theta_1 + G_c C_1 + \frac{\partial^2 u_1}{\partial y^2} - \frac{u_1}{K_p} + \frac{B u_0}{K_p}, \quad (19)$$

$$-\omega \theta_1 - A \frac{\partial \theta_0}{\partial y} - \frac{\partial \theta_1}{\partial y} = \frac{1}{P_r} \frac{\partial^2 \theta_1}{\partial y^2} - F \theta_1, \quad (20)$$

$$-\omega C_1 - A \frac{\partial C_0}{\partial y} - \frac{\partial C_1}{\partial y} = \frac{1}{S_c} \frac{\partial^2 C_1}{\partial y^2}. \quad (21)$$

The corresponding boundary conditions are

$$u_0 = \alpha_1 + h_1 \frac{\partial u_0}{\partial y}, u_1 = h_1 \frac{\partial u_1}{\partial y}, \frac{\partial \theta_0}{\partial y} = -1, \frac{\partial \theta_1}{\partial y} = 0, \frac{\partial C_0}{\partial y} = -1, \frac{\partial C_1}{\partial y} = 0 \quad \text{at } y = 0, \\ u_0 = \alpha_2 + h_2 \frac{\partial u_0}{\partial y}, u_1 = h_2 \frac{\partial u_1}{\partial y}, \theta_0 = 0, \theta_1 = 0, C_0 = 0, C_1 = 0 \quad \text{at } y = 1. \quad (22)$$

The solutions of Equations (16)-(21) under boundary condition (22) are given by

$$u(y, t) = (B_1 e^{m_1 y} + B_2 e^{m_2 y} - B_8 e^{\lambda_3 y} - B_9 e^{\lambda_4 y} - B_{10} e^{-S_c y} + B_{11}) + \varepsilon e^{-\omega t} (B_3 e^{m_3 y} + B_4 e^{m_4 y} - B_{12} e^{\lambda_1 y} \\ - B_{13} e^{\lambda_2 y} + D_0 e^{\lambda_3 y} + D_1 e^{\lambda_4 y} - D_2 e^{\lambda_5 y} - D_3 e^{\lambda_6 y} - D_4 e^{m_1 y} - D_5 e^{m_2 y} - D_6 e^{-S_c y}), \quad (23)$$

$$\theta(y, t) = (A_2 e^{\lambda_3 y} + A_3 e^{\lambda_4 y}) + \varepsilon e^{-\omega t} (A_4 e^{\lambda_5 y} + B_0 e^{\lambda_6 y} - B_6 e^{\lambda_3 y} - B_7 e^{\lambda_4 y}), \quad (24)$$

$$C(y, t) = \frac{1}{S_c} (e^{-S_c y} + e^{S_c}) + \varepsilon e^{-\omega t} (A_0 e^{\lambda_1 y} + A_1 e^{\lambda_2 y} + B_5 e^{-S_c y}). \quad (25)$$

The wall shear stress i.e. the skin friction at the wall is given by

$$\tau = \left( \frac{\partial u}{\partial y} \right)_{y=0} = \left( \frac{\partial u_0}{\partial y} \right)_{y=0} + \varepsilon e^{-\omega t} \left( \frac{\partial u_1}{\partial y} \right)_{y=0}. \quad (26)$$

Using Equation (23) in Equation (26), it is given by

$$\tau = (m_1 B_1 + m_2 B_2 - \lambda_3 B_8 - \lambda_4 B_9 + S_c B_{10}) + \varepsilon e^{-\omega t} (m_3 B_3 + m_4 B_4 - \lambda_1 B_{12} \\ - \lambda_2 B_{13} + \lambda_3 D_0 + \lambda_4 D_1 - \lambda_5 D_2 - \lambda_6 D_3 - m_1 D_4 - m_2 D_5 + S_c D_6). \quad (27)$$

The rate of heat transfer i.e. the heat flux at the wall is given by

$$N_u = \left( \frac{\partial \theta}{\partial y} \right)_{y=0} = \left( \frac{\partial \theta_0}{\partial y} \right)_{y=0} + \varepsilon e^{-\omega t} \left( \frac{\partial \theta_1}{\partial y} \right)_{y=0}. \quad (28)$$

Using Equation (24) in Equation (28), it is given by

$$N_u = (\lambda_3 A_2 + \lambda_4 A_3) + \varepsilon e^{-\omega t} (\lambda_5 A_4 + \lambda_6 B_0 - \lambda_3 B_6 - \lambda_4 B_7), \quad (29)$$

where

$$\lambda_1 = -\frac{S_c}{2} + \frac{1}{2} \sqrt{S_c^2 - 4\omega S_c}, \quad \lambda_2 = -\frac{S_c}{2} - \frac{1}{2} \sqrt{S_c^2 - 4\omega S_c}, \quad \lambda_3 = -\frac{Pr}{2} + \frac{1}{2} \sqrt{Pr^2 + 4PrF}, \\ \lambda_4 = -\frac{Pr}{2} - \frac{1}{2} \sqrt{Pr^2 + 4PrF}, \quad \lambda_5 = -\frac{Pr}{2} + \frac{1}{2} \sqrt{Pr^2 - 4Pr(\omega - F)}, \quad \lambda_6 = -\frac{Pr}{2} - \frac{1}{2} \sqrt{Pr^2 - 4Pr(\omega - F)},$$

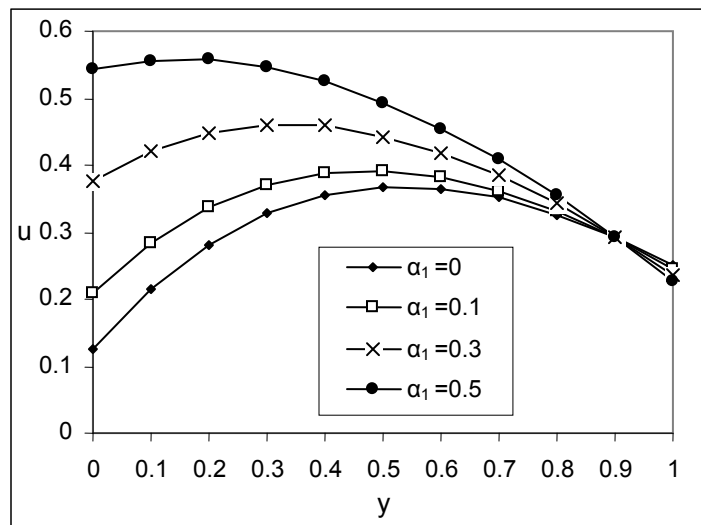
$$\begin{aligned}
 m_1 &= -\frac{1}{2} + \frac{1}{2} \sqrt{1 + \frac{4}{K_p}}, m_2 = -\frac{1}{2} - \frac{1}{2} \sqrt{1 + \frac{4}{K_p}}, m_3 = -\frac{1}{2} + \frac{1}{2} \sqrt{1 + 4 \left( \frac{1}{K_p} - \omega \right)}, m_4 = -\frac{1}{2} - \frac{1}{2} \sqrt{1 + 4 \left( \frac{1}{K_p} - \omega \right)}, \\
 A_0 &= \frac{(B_5 S_c e^{\lambda_2} + B_5 \lambda_2 e^{-S_c})}{(\lambda_1 e^{\lambda_2} - \lambda_2 e^{\lambda_1})}, A_1 = \frac{(B_5 S_c - A_0 \lambda_1)}{\lambda_2}, A_2 = \frac{e^{\lambda_4}}{(\lambda_4 e^{\lambda_3} - \lambda_3 e^{\lambda_4})}, A_3 = -\frac{A_2 e^{\lambda_3}}{e^{\lambda_4}}, \\
 A_4 &= \frac{e^{\lambda_6} (B_6 \lambda_3 + B_7 \lambda_4) - \lambda_6 (B_6 e^{\lambda_3} + B_7 e^{\lambda_4})}{(\lambda_5 e^{\lambda_6} - \lambda_6 e^{\lambda_5})}, B_0 = \frac{B_6 \lambda_3 + B_7 \lambda_4 - A_4 \lambda_5}{\lambda_6}, B_1 = \frac{E_3 E_5 - E_2 E_6}{E_1 E_5 - E_2 E_4}, \\
 B_2 &= \frac{E_3 - B_1 E_1}{E_2}, B_3 = \frac{E_9 E_{11} - E_8 E_{12}}{E_7 E_{11} - E_8 E_{10}}, B_4 = \frac{E_9 - B_3 E_7}{E_8}, B_5 = -\frac{A}{\omega S_c}, B_6 = \frac{AP_r A_2 \lambda_3}{\lambda_3^2 + \lambda_3 P_r + P_r (\omega - F)}, \\
 B_7 &= \frac{AP_r A_3 \lambda_4}{\lambda_4^2 + \lambda_4 P_r + P_r (\omega - F)}, B_8 = \frac{G_r A_2}{\lambda_3^2 + \lambda_3 - \frac{1}{K_p}}, B_9 = \frac{G_r A_3}{\lambda_4^2 + \lambda_4 - \frac{1}{K_p}}, B_{10} = \frac{G_c}{S_c \left( S_c^2 - S_c - \frac{1}{K_p} \right)}, \\
 B_{11} &= \frac{G_c K_p e^{-S_c}}{S_c}, B_{12} = \frac{G_c A_0}{\lambda_1^2 + \lambda_1 - \left( \frac{1}{K_p} - \omega \right)}, B_{13} = \frac{G_c A_1}{\lambda_2^2 + \lambda_2 - \left( \frac{1}{K_p} - \omega \right)}, D_0 = \frac{G_r B_6 + AB_8 \lambda_3 + \frac{BB_8}{K_p}}{\lambda_3^2 + \lambda_3 - \left( \frac{1}{K_p} - \omega \right)}, \\
 D_1 &= \frac{G_r B_7 + AB_9 \lambda_4 + \frac{BB_9}{K_p}}{\lambda_4^2 + \lambda_4 - \left( \frac{1}{K_p} - \omega \right)}, D_2 = \frac{G_r A_4}{\lambda_5^2 + \lambda_5 - \left( \frac{1}{K_p} - \omega \right)}, D_3 = \frac{G_r B_0}{\lambda_6^2 + \lambda_6 - \left( \frac{1}{K_p} - \omega \right)}, \\
 D_4 &= \frac{AB_1 m_1 + \frac{BB_1}{K_p}}{m_1^2 + m_1 - \left( \frac{1}{K_p} - \omega \right)}, D_5 = \frac{AB_2 m_2 + \frac{BB_2}{K_p}}{m_2^2 + m_2 - \left( \frac{1}{K_p} - \omega \right)}, D_6 = \frac{\frac{BB_{10}}{K_p} - AB_{10} S_c - G_c B_5}{S_c^2 - S_c - \left( \frac{1}{K_p} - \omega \right)}, D_7 = \frac{BB_{11}}{K_p \left( \frac{1}{K_p} - \omega \right)}, \\
 E_1 &= 1 - h_1 m_1, E_2 = 1 - h_1 m_2, E_3 = \alpha_1 + B_8 (1 - h_1 \lambda_3) + B_9 (1 - h_1 \lambda_4) + B_{10} (1 + h_1 S_c) - B_{11}, \\
 E_4 &= e^{m_1} (1 - h_2 m_1), E_5 = e^{m_2} (1 - h_2 m_2), \\
 E_6 &= \alpha_2 + B_8 e^{\lambda_5} (1 - h_2 \lambda_3) + B_9 e^{\lambda_4} (1 - h_2 \lambda_4) + B_{10} e^{-S_c} (1 - h_2 S_c) - B_{11}, E_7 = 1 - h_1 m_3, E_8 = 1 - h_1 m_4, \\
 E_9 &= B_{12} (1 - h_1 \lambda_1) + B_{13} (1 - h_1 \lambda_2) - D_0 (1 - h_1 \lambda_3) - D_1 (1 - h_1 \lambda_4) + D_2 (1 - h_1 \lambda_5) \\
 &+ D_3 (1 - h_1 \lambda_6) + D_4 (1 - h_1 m_1) + D_5 (1 - h_1 m_2) + D_6 (1 + h_1 S_c) + D_7, E_{10} = e^{m_3} (1 - h_2 m_3), \\
 E_{11} &= e^{m_4} (1 - h_2 m_4), \\
 E_{12} &= B_{12} e^{\lambda_1} (1 - h_2 \lambda_1) + B_{13} e^{\lambda_2} (1 - h_2 \lambda_2) - D_0 e^{\lambda_3} (1 - h_2 \lambda_3) - D_1 e^{\lambda_4} (1 - h_2 \lambda_4) + D_2 e^{\lambda_5} (1 - h_2 \lambda_5) \\
 &+ D_3 e^{\lambda_6} (1 - h_2 \lambda_6) + D_4 e^{m_1} (1 - h_2 m_1) + D_5 e^{m_2} (1 - h_2 m_2) + D_6 e^{-S_c} (1 + h_2 S_c) + D_7. \tag{30}
 \end{aligned}$$

#### 4. Discussions and Results

This paper discusses the effect of variable suction and mass transfer on unsteady free convective couette flow of a viscous incompressible fluid in the slip flow regime in presence of variable suction and radiative heat source. The governing equations of the flow field are solved for the velocity, temperature, concentration distribution, skin friction and the rate of heat transfer and the effects of the various flow parameters on the flow field have been studied and the results are presented graphically and discussed quantitatively with the aid of velocity profiles 1-9, temperature profiles 10-11 and concentration distribution shown in Figure 12.

#### 4.1. Velocity field

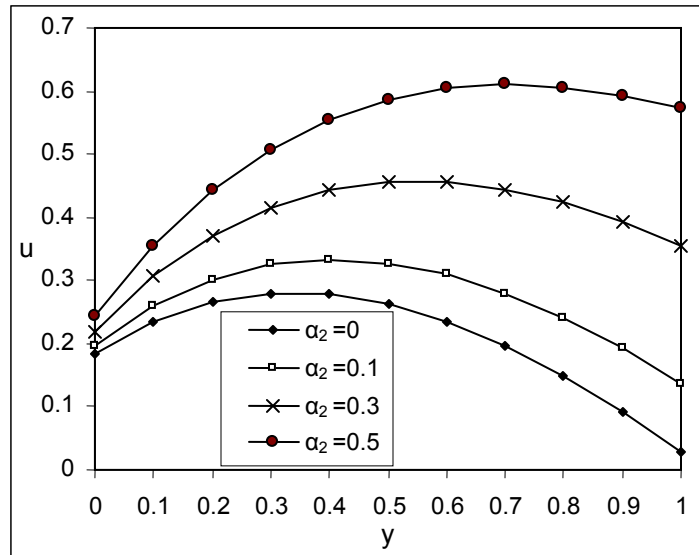
The velocity of the flow field varies to a great extent with the variation of the flow parameters. The main factors affecting the velocity of the flow field are suction parameters  $\alpha_1, \alpha_2$ , Grashof number for heat and mass transfer  $G_r, G_c$ ; slip flow parameters  $h_1, h_2$ , radiation parameter  $F$ , permeability parameter  $K_p$  and Schmidt number  $S_c$ . The effects of these parameters on the velocity of the flow field are analyzed in Figures 1-9.



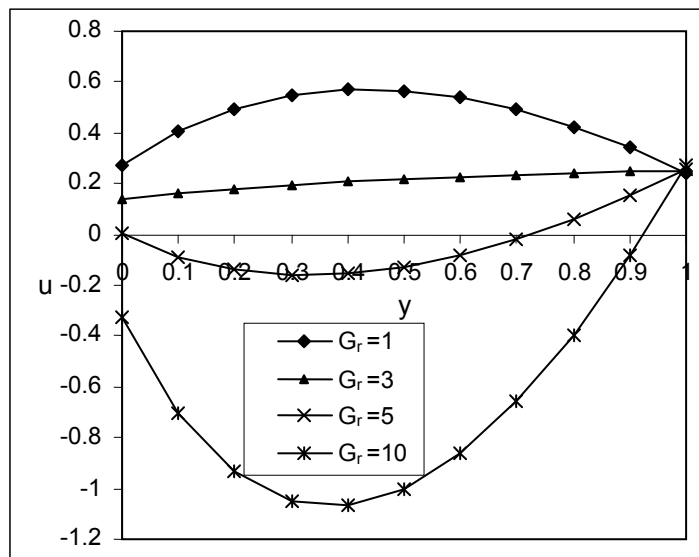
**Figure 1:** Velocity profiles against  $y$  for different values of  $\alpha_1$  with  $P_r=0.71, \omega=0.1, t=0.1, \epsilon=0.02, G_c=2, G_r=2, S_c=0.6, K_p=1, F=0.1, A=0.5, B=0.5, h_1=0.1, h_2=0.1$  and  $\alpha_2=0.2$

Figures 1 and 2 discuss the effect of suction parameters  $\alpha_1$  and  $\alpha_2$  respectively on the flow field. Analyzing the curves of both the figures, it is observed that both the parameters have accelerating effect on the velocity of the flow field at all points. Figures 3 and 4 respectively depict the effect of Grashof number for heat transfer  $G_r$  and mass transfer  $G_c$  on the flow field. The Grashof number for heat transfer is found to retard the velocity of the flow field at all points. The effect of a growing Grashof number for mass transfer is to accelerate the magnitude of velocity of the flow field at all points. The effects of slip flow parameters  $h_1, h_2$ ; on the velocity of the flow field are shown in Figures 5 and 6 respectively. Comparing the curves of both the figures, it is observed that both the parameters enhance the velocity of the flow field at all points in a different manner. The parameter  $h_1$  tends to converge the velocity profiles at a point and there after the effect reverses while the parameter  $h_2$  tends to diverge the velocity profiles from a point.

Figure 7 shows the effect of radiation parameter  $F$  on the flow field. A growing radiation parameter is found to accelerate the velocity of the flow field at all points. In Figure 8, we present the effect of permeability parameter  $K_p$  on the velocity field. The effect of increasing permeability parameter is to accelerate the velocity of the flow field at all points. Figure 9 elucidates the effect of Schmidt number  $S_c$  on the velocity field. The effect of growing  $S_c$  is to decrease the velocity at all points of the flow field.

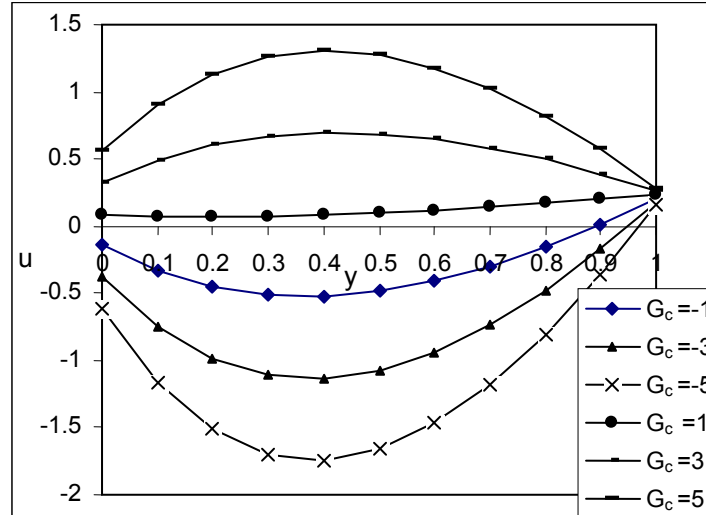


**Figure 2:** Velocity profiles against  $y$  for different values of  $\alpha_2$  with  $P_r=0.71$ ,  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$ ,  $G_c=2$ ,  $G_r=2$ ,  $S_c=0.6$ ,  $K_p=1$ ,  $F=0.1$ ,  $A=0.5$ ,  $B=0.5$ ,  $h_1=0.1$ ,  $h_2=0.1$  and  $\alpha_1=0.1$

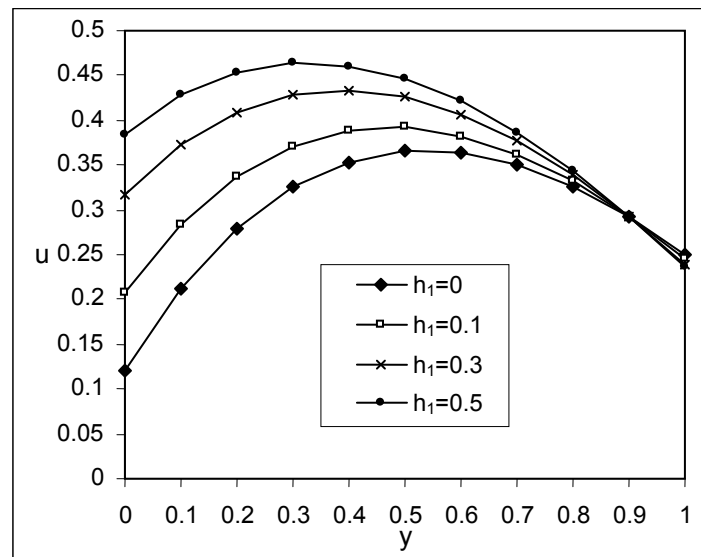




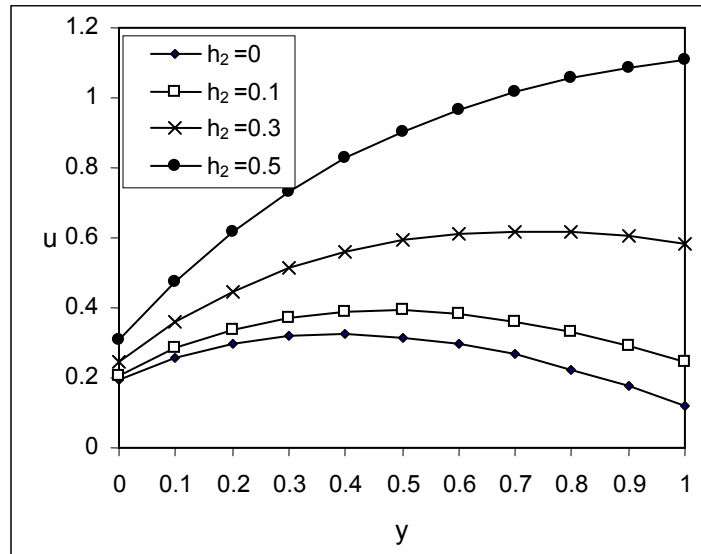
**Figure 3:** Velocity profiles against  $y$  for different values of  $G_r$  with  $P_r=0.71$ ,  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$ ,  $G_c=2$ ,  $S_c=0.6$ ,  $K_p=1$ ,  $F=0.1$ ,  $A=0.5$ ,  $B=0.5$ ,  $h_1=0.1$ ,  $h_2=0.1$ ,  $\alpha_1=0.1$  and  $\alpha_2=0.2$



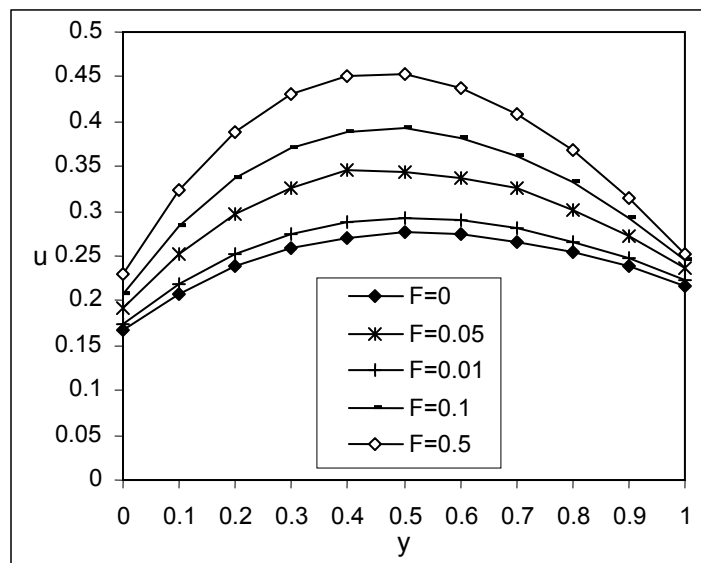
**Figure 4:** Velocity profiles against  $y$  for different values of  $G_c$  with  $P_r=0.71$ ,  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$ ,  $G_r=2$ ,  $S_c=0.6$ ,  $K_p=1$ ,  $F=0.1$ ,  $A=0.5$ ,  $B=0.5$ ,  $h_1=0.1$ ,  $h_2=0.1$ ,  $\alpha_1=0.1$  and  $\alpha_2=0.2$



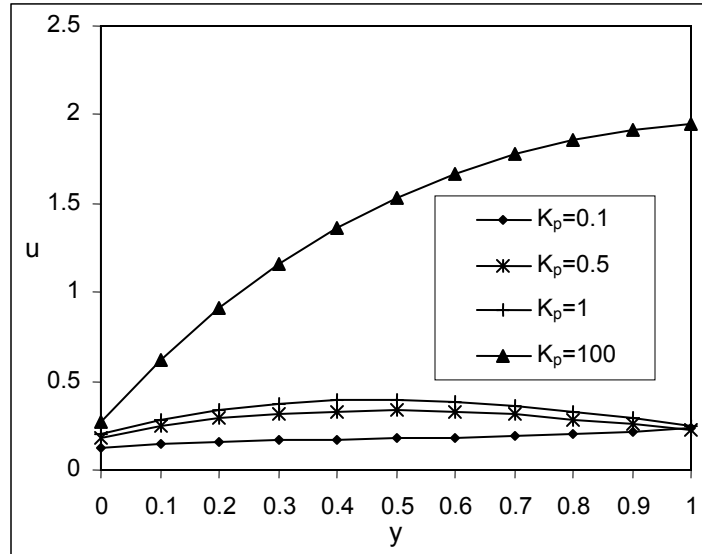
**Figure 5:** Velocity profiles against  $y$  for different values of  $h_1$  with  $P_r=0.71$ ,  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$ ,  $G_c=2$ ,  $G_r=2$ ,  $S_c=0.6$ ,  $K_p=1$ ,  $F=0.1$ ,  $A=0.5$ ,  $B=0.5$ ,  $h_2=0.1$ ,  $\alpha_1=0.1$  and  $\alpha_2=0.2$



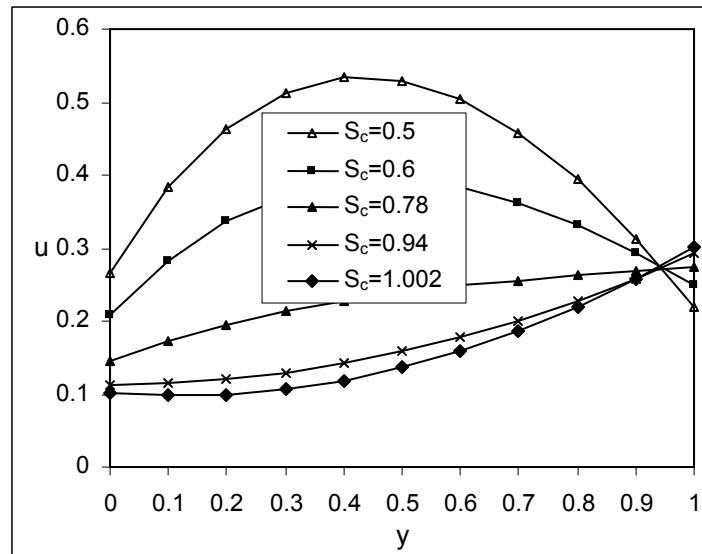
**Figure 6:** Velocity profiles against y for different values of  $h_2$  with  $P_r=0.71$ ,  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$ ,  $G_c=2$ ,  $G_r=2$ ,  $S_c=0.6$ ,  $K_p=1$ ,  $F=0.1$ ,  $A=0.5$ ,  $B=0.5$ ,  $h_1=0.1$ ,  $\alpha_1=0.1$  and  $\alpha_2=0.2$



**Figure 7:** Velocity profiles against y for different values of F with  $P_r=0.71$ ,  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$ ,  $G_c=2$ ,  $G_r=2$ ,  $S_c=0.6$ ,  $K_p=1$ ,  $A=0.5$ ,  $B=0.5$ ,  $h_1=0.1$ ,  $h_2=0.1$ ,  $\alpha_1=0.1$  and  $\alpha_2=0.2$



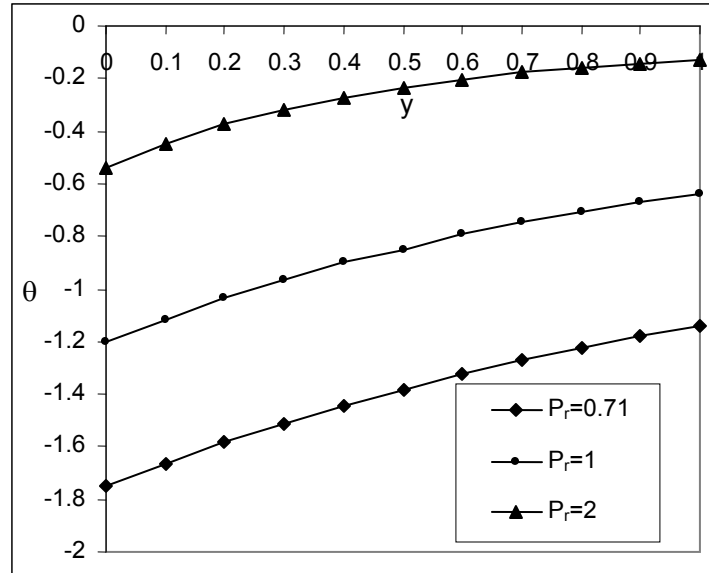
**Figure 8:** Velocity profiles against  $y$  for different values of  $K_p$  with  $P_r=0.71$ ,  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$ ,  $G_c=2$ ,  $G_r=2$ ,  $S_c=0.6$ ,  $F=0.1$ ,  $A=0.5$ ,  $B=0.5$ ,  $h_1=0.1$ ,  $h_2=0.1$ ,  $\alpha_1=0.1$  and  $\alpha_2=0.2$



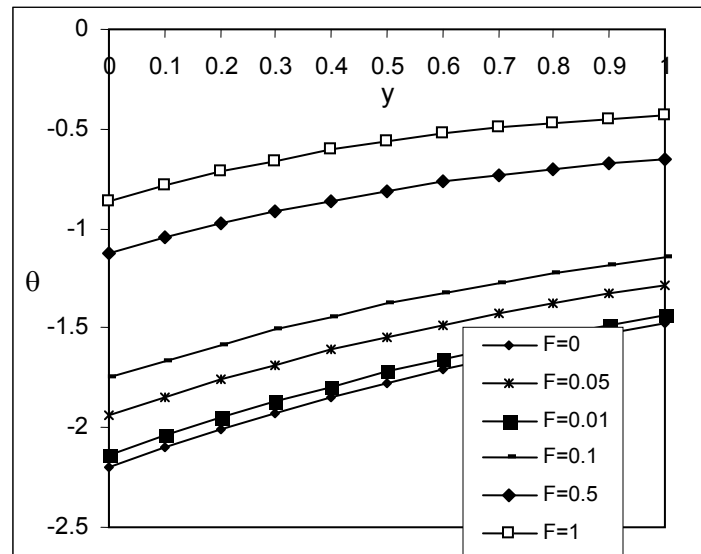
**Figure 9:** Velocity profiles against  $y$  for different values of  $S_c$  with  $P_r=0.71$ ,  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$ ,  $G_c=2$ ,  $G_r=2$ ,  $K_p=1$ ,  $F=0.1$ ,  $A=0.5$ ,  $B=0.5$ ,  $h_1=0.1$ ,  $h_2=0.1$ ,  $\alpha_1=0.1$  and  $\alpha_2=0.2$

#### 4.2. Temperature field

The temperature field suffers a major change in magnitude due to the variation of Prandtl number  $P_r$  and radiation parameter  $F$ . The effects of these parameters on the temperature field are discussed in Figures 10-11. Both the parameters retard the magnitude of temperature of the flow field at all points.



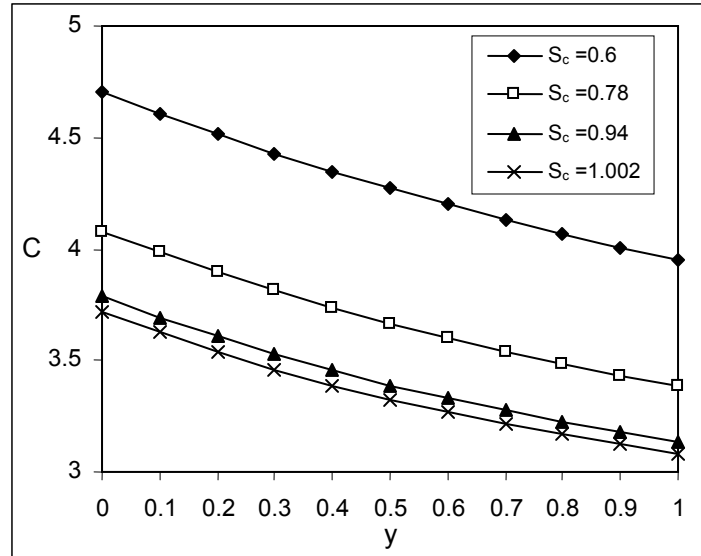
**Figure 10:** Temperature profiles against  $y$  for different values of  $P_r$  with  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$ ,  $F=0.1$  and  $A=0.5$



**Figure 11:** Temperature profiles against  $y$  for different values of  $F$  with  $P_r=0.71$ ,  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$  and  $A=0.5$

### 4.3. Concentration distribution

The presence of foreign mass in the flow field greatly affects the concentration boundary layer thickness of the flow field at all points. The factor responsible for this variation is Schmidt number  $S_c$ . In Fig.12, keeping other parameters of the flow field constant, the Schmidt number  $S_c$  is varied in steps and its effect on the concentration boundary layer of the flow field is studied. It is observed that a growing Schmidt number reduces the concentration boundary layer of the flow field at all points.



**Figure 12:** Concentration profiles against  $y$  for different values of  $S_c$  with  $\omega=0.1$ ,  $t=0.1$ ,  $\epsilon=0.02$  and  $A=0.5$

## 5. Conclusions

We present below some of the important features of the flow field due to the variation of the flow parameters.

1. Both the suction parameters  $\alpha_1$  and  $\alpha_2$  are observed to have an accelerating effect on the velocity of the flow field at all points.
2. The Grashof number for heat transfer  $G_r$  is found to retard the velocity of the flow field at all points and the effect of a growing Grashof number for mass transfer  $G_c$  is to accelerate the magnitude of velocity of the flow field at all points.
3. The slip flow parameters  $h_1$  and  $h_2$  enhance the velocity of the flow field at all points in a different manner. The parameter  $h_1$  tends to converge the velocity profiles at a point and there after the effect reverses while the parameter  $h_2$  tends to diverge the velocity profiles from a point.
4. A growing radiation parameter  $F$  is found to accelerate the velocity of the flow field at all points.
5. The effect of increasing permeability parameter  $K_p$  is to accelerate the velocity of the flow field at all points.
6. The Prandtl number  $P_r$  and the radiation parameter  $F$  retard the magnitude of temperature of the flow field at all points.
7. A growing Schmidt number reduces the concentration boundary layer thickness of the flow field at all points.

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